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Removal of Surfactant from Nanocomposites Films Based on Thermally Reduced Graphene Oxide and Natural Rubber

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Abstract: Electrically conducting elastomer composites based on natural rubber and reduced graphene oxide (rGO) is reported. These composites were prepared by a latex method and an easy washing process. The latex method consists of the mixing of an aqueous suspension of rGO, stabilized by sodium dodecyl sulfate and pre-vulcanized natural rubber, followed by solvent casting. The percolation threshold of composites was estimated at 1.54 wt.% of rGO. The washing process allowed elimination of the surfactant completely from nanocomposites. The absence of surfactant in nanocomposites was demonstrated by Raman spectroscopy and dynamo-mechanical analysis. The surfactant-free nanocomposites showed improved mechanical and electrical properties.

Keywords: thermally reduced graphene oxide; natural rubber latex; electrical properties; mechanical properties

1. Introduction

The advancement in the field of carbon polymorphs, such as carbon nanotubes and graphene, has significantly contributed to the development of new composites with different applications [1–6]. In the case of elastomers, electrically conducting rubber nanocomposites can be prepared by using carbon-based nanomaterials, such as graphene materials, as a filler [7]. These types of graphene materials can be prepared by diverse methods [8–10], however, the thermal reduction of graphite oxide (rGO) is considered as one of the easiest method [11,12]. Mastication, latex mixing and solution casting are the most used methods for the preparation of rubber nanocomposites. In the case of the latex method, this is carried out by using natural rubber latex and stable suspensions of graphene. There are some studies reported in the literature concerning the effect of graphene on the natural rubber latex properties [7,13–21]. In most of these studies, aqueous suspensions of graphene were incorporated in natural rubber latex followed by precipitation or drying the mixture, and a further vulcanization process using rollers or solvents over extended periods of time. Although these studies indicate the use of different strategies to improve graphene dispersion in the polymer matrix, few of them report how the properties of the resulting composites are affected by the presence of additives, such as surfactants. The aqueous suspensions of graphene are generally obtained by using surfactants, which are compounds of amphipathic character. Surfactants impart colloidal stability of hydrophobic



materials, such as graphene, in water. The stabilization of graphene aqueous suspensions has been studied through the use of ionic and non-ionic surfactants. In the case of ionic surfactants, its use would achieve better suspension stabilization if the surfactant concentration was higher than or closer to the critical micelle concentration [22]. In the case of non-ionic surfactants, the concentration of graphene sheets coated with a surfactant is related linearly with a steric originated repulsive potential barrier. A high steric potential facilitates graphene dispersion in aqueous suspension [23]. Sodium dodecyl sulfate (SDS) is a low-cost commercially available anionic surfactant, which has been extensively studied for the preparation of stable water suspensions of graphene. These stable suspensions are proper for dispersing graphene in latexes of different polymers, especially rubber latex. This is due to the fact that the low viscosity of rubber latex allows an optimal dispersion, compared to mastication or roll milling methods. However, the addition of a surfactant alters the final composition and properties of the composites. As we previously reported, the use of SDS promotes the attainment of better colloidal stability to prepare rGO/natural rubber composites, while dodecyltrimethylamonium bromide (DTAB) promotes slight flocculation of natural rubber particles [18]. It is also possible to increase the electrical conductivity of natural rubber from 10^{-14} S/m to 4.9×10^{-2} S/m, when 4% rGO is used as the filler [20]. However, the elongation at the break was reduced drastically. Microdomains of surfactant in rubber composites could be the result of a high content of surfactant. These microdomains act as defect centers, producing the failure of the materials under mechanical stress.

The electrical percolation of carbon-based nanomaterials/rubber composites is explained by the percolation theory. This theory corresponds to a statistical physics model represented as the random connectivity of adjacent sites of hard-core circles, or cylinder or layer in an infinite periodic lattice [24–26]. The electrical conductivity measured in composites based on electrically conducting fillers and insulating polymer matrices is attributed to the formation of a three-dimensional interconnected network of the conductive phase. The critical filler content, where the composite becomes electrically conductive, is known as the percolation threshold (ϕ_C) [27]. The electron mobility of electrons is attributed to the tunneling between adjacent carbon particles improved by thermal fluctuations [28,29]. Hence, the presence of a surfactant surrounding the graphene in elastomer composites can affect the charge mobility, impeding the achievement of the optimal performance of electrical conductivity of the composites based on natural rubber and terminally reduced graphene oxide. The elimination of the surfactant from the rGO/natural rubber and rGO, favoring the improvement of the mechanical properties.

2. Experimental

2.1. Materials

Double-centrifuged pre-vulcanized natural rubber latex (NR) with high ammonia content and with a total solid content of 56.87% (49.08% of natural rubber), kindly supplied by TECNILATEX S.A. (Alcorcón, Madrid, Spain), was used. Reduced graphite oxide (rGO) was produced by a thermal reduction process of graphite oxide at 1000 °C under an argon atmosphere [7]. The graphite oxide was synthesized from natural graphite by the method of Brodie [30]. A thorough characterization of the material has been already reported [12]. The SDS supplied from Sigma-Aldrich was used as received.

2.2. Preparation of NR/rGO and w-NR/rGO Nanocomposites

The aqueous suspension of rGO was prepared by using a 1 wt.% SDS solution, where the concentration of rGO was 0.3 wt.%. The rGO was dispersed by sonication for 1 h. Known volumes of the rGO suspensions were added to pre-vulcanized natural rubber latex to obtain nanocomposites containing between 1–4 wt.% of rGO. Afterward, the samples were dried for 24 h at 70 °C and were designated as NR/rGO samples. The washing process of NR/rGO composites consisted in introducing the composite film in a 250 mL flask containing 200 mL of distilled water and was left stirring for 72 h.

Then, the film was removed, washed with distilled water and dried for 12 h at 70 $^{\circ}$ C. These samples were termed w-NR/rGO.

2.3. Nanocomposite Characterization

The nanocomposites were characterized by Raman spectroscopy, using a Renishaw Invia Raman microscope with a laser wavelength of 514.5 nm and a spectral resolution of 0.02 cm^{-1} . Mechanical tests were carried out at room temperature and a pulling speed of 500 mm·min⁻¹, using an Instron model 3366 dynamometer according to ASTM D 412 specifications. The results are the average of at least five measurements for each sample.

The degree of dispersion of the rGO layers and nanocomposite morphology were analyzed by transmission electron microscopy (TEM) using a Philips Tecnai 20 transmission electron microscope with an acceleration voltage of 200 kV. Samples of ultra-thin sections were prepared by cryoultramicrotomy at -140 °C, using a Leica EM UC6 cryoultramicrotome ((Leica, Vienna, Austria).

The dynamic mechanical analysis was carried out using a Mettler Toledo 861e DMA. The tension mode was 1 Hz and the temperature range was between -100 and 0 °C, with a heating rate of 2 °C·min⁻¹. The experimental error was less than 5%. The electrical conductivity of the nanocomposites was measured on a high-resolution Alpha-Novocontrol dielectric spectrometer. The films were placed in the dielectric cell between two parallel gold electrodes. The conductivity measurement was given directly by the analyzer.

3. Results and Discussion

3.1. Raman Spectroscopy

The Raman spectra of natural rubber (NR) and washed NR (w-NR) are shown in Figure 1. An intense band at 1666 cm⁻¹ was observed, which corresponded to the C=C stretching. Other characteristic bands of natural rubber were seen, such as 1444 cm⁻¹, 1368 cm⁻¹ and 993 cm⁻¹, which corresponded to CH₂ deformation, CH₃ asymmetric deformation and C-CH₂ stretching, respectively [31]. No significant changes were observed as a consequence of the washing of the NR film with water. This indicated that, despite the washing of the film, the natural rubber did not present a significant change in its composition. Figure 2 shows the Raman spectra of the natural rubber/rGO composites and washed natural rubber/rGO composite, where the characteristic D and G bands of the graphene materials were observed. In the case of washed composites, a Raman red-shift for the band associated with C=C stretching of the NR was observed. Simultaneously, the G and D bands presented a Raman blue-shift. These facts suggested that the elimination of the surfactant was successful, favoring interactions between the natural rubber backbone and the reduced graphene oxide.

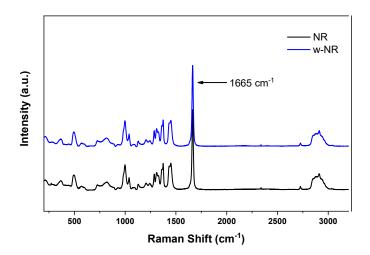


Figure 1. Raman spectra of natural rubber (NR) and washed (w)-NR.

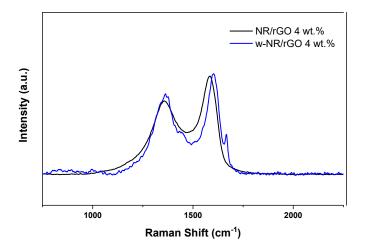


Figure 2. Raman spectra of natural rubber/reduced graphene oxide (NR/rGO) 4.0 wt.% and w-NR/rGO 4.0 wt.%.

3.2. Electrical Conductivity of NR/rGO Nanocomposites

The electrical conductivity measured at 1 Hz, as a function of the rGO content, is shown in Figure 3. It was observed that the electrical conductivity of NR is 2.66×10^{-10} S/m, which is characteristic of electrically insulating materials. The electrical conductivity increased up to 9.06×10^{-5} S/m with 4 wt.% of rGO content, as a consequence of the addition of reduced graphene oxide to the natural rubber. The percolation threshold of rGO was around 2.50 wt.%. In the case of the washed nanocomposites, it was observed that the electrical conductivity of each composite partially increased. The electrical conductivity of composites with 4 wt.% achieved a value of 6.16×10^{-5} S/m and the percolation threshold decreased, reaching a value of 1.54 wt.%. This increase could be attributed to the fact that small SDS molecules occupy the free volume, inhibiting the tunneling of an electron between the reduced graphene oxide layers. As a consequence of the elimination of SDS, an increase of the electrical conductivity was achieved. In this respect, the effect of small molecules—such as the solvent on the electrical properties of carbon-based elastomer composites—was reported by Pavlovsky and Siegmann [32], who demonstrated that the reversible swelling of carbon-based composites allows the occurrence of the breakdown and reconstruction of the filler conducting network. The electrical conductivity observed in w-NR/rGO could be attributed mainly by the occurrence of tunneling between the adjacent rGO layers, since there is a predominance of electronic conductivity. It is interesting to note that in the literature, there are other materials, which present similar orders of electrical conductivity, such as those nanocomposites based on polymer electrolytes. However, the electrical conductivity of these types of composites is attributed to ionic conductivity [33,34].

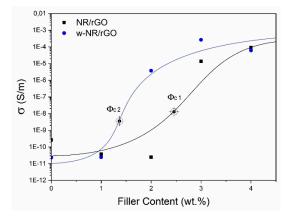


Figure 3. Electrical conductivity of NR/rGO and w-NR/rGO composites as a function of the rGO content.

3.3. Mechanical Properties of NR/Reduced Graphene Oxide Composites

Table 1 presents the modulus at 100% and 300% of elongation, the ultimate tensile strength and elongation at break of the NR and nanocomposites. As expected, the addition of rGO to NR promoted the increase of stiffness of the resulting nanocomposites. This could be attributed to the fact that the filler partially occupies the free volume fraction, inhibiting the free rotation of polymer chains. In addition, the increase of the filler (rGO) content produced a decrease of the elongation at break of the composite. This fact was related to the presence of filler, which induced defects in the composites. An interesting fact was observed as a consequence of the washing process. The w-NR/rGO samples with contents of 1 wt.%, 2 wt.% and 3 wt.% of rGO presented a lower E100 modulus. This fact could be related to the elimination of the surfactant from the nanocomposites as a result of the washing process. In addition, washed composites presented a tendency to have higher ultimate tensile strength than unwashed composites. This could be attributed to the fact that the elimination of the surfactant molecules allowed the natural rubber chains to be in closer contact with the filler, which improved their interactions. Likewise, the elimination of the surfactant could reduce the surfactant microdomains, which can act as failure centers in composites films.

Table 1. Modulus at 100% and 300% of elongation,	ultimate tensile strength and elongation at break of
NR/rGO and w-NR/rGO composites.	

Sample	Modulus E100 (MPa)	Modulus E300 (MPa)	Ultimate Tensile Strength (MPa)	Elongation at Break (%)
NR	0.80	1.53	19.5	754
NR/rGO1wt.%	1.07	2.74	25.2	674
NR/rGO 2 wt.%	1.52	4.37	22.1	596
NR/rGO 3 wt.%	2.14	6.07	24.1	602
NR/rGO 4 wt.%	1.93	5.49	15.9	495
w-NR/rGO1wt.%	0.96	2.44	24.9	691
w-NR/rGO 2 wt.%	1.52	4.70	24.8	620
w-NR/rGO3wt.%	1.95	6.17	19.4	526
w-NR/rGO 4 wt.%	2.48	7.44	19.3	423

3.4. Morphology of NR/Reduced Graphene Oxide Composites

Figure 4 shows the TEM images of NR/rGO 3 wt.% and w-NR/rGO 3 wt.%. In the case of NR/rGO, it was observed that the layers of reduced graphene oxide were dispersed in an elastomeric matrix. However, there were zones were the rGO layers appeared partially stacked and the formation of a filler network was observed. Previously, it has been reported that in natural rubber composites filled with graphene prepared by using the latex method, the graphene layers tended to occupy the interstices between the NR particles [7]. This indicates that although the surfactant enhances the stability of graphene in an aqueous suspension, the dispersion of the reduced graphene oxide layers will be affected by the characteristic of the NR particles and their stability. As a result of the washing process, the rGO layers appeared more dispersed in the elastomer matrix. This suggested that a higher interaction between the rGO layers and polymer matrix can take place as the consequence of the elimination of the surfactant by using the washing process.

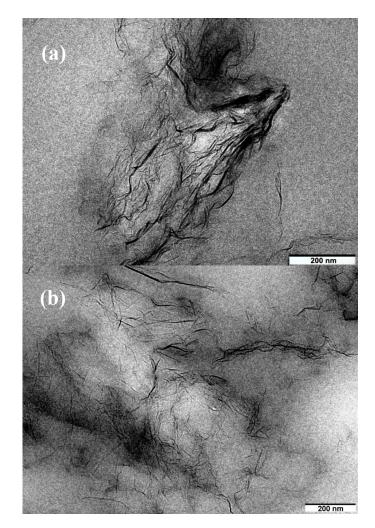


Figure 4. Transmission electron microscopy of NR/rGO 3 wt.% (a) and w-NR/rGO 3wt.% (b).

3.5. Dynamo-Mechanical of NR/Reduced Graphene Oxide Composites

A dynamo-mechanical analysis provides information on the viscoelastic properties of materials, where the elastic portion is represented by the storage modulus and the viscous portion is represented by the loss modulus. Figures 5 and 6 present the storage modulus and loss modulus, respectively, of NR, NR / rGO 4 wt.% and w-NR / rGO 4 wt.% in the temperature range of -80 °C to -30 °C. It was observed that the storage modulus of all samples showed a fall around -60 °C, which corresponded to the glass transition temperature of NR [7]. The addition, the SDS-dispersed rGO produced a storage modulus increase of around -50 °C, which could indicate that the SDS molecules affect the cooperative movement of the natural rubber backbone. This was also observed in the loss modulus of NR/rGO 4 wt.%, where a bimodal peak was observed. The presence of SDS did not significantly alter the glass transition temperature (Tg) of NR, but its presence produced a composite that could present partial heterogeneity. Instead, the w-NR/rGO 4 wt.% presented storage and the loss modulus shifted to a higher temperature. This suggested that the washing process eliminated the surfactant from the nanocomposite, which promoted the interaction between rGO and natural rubber.

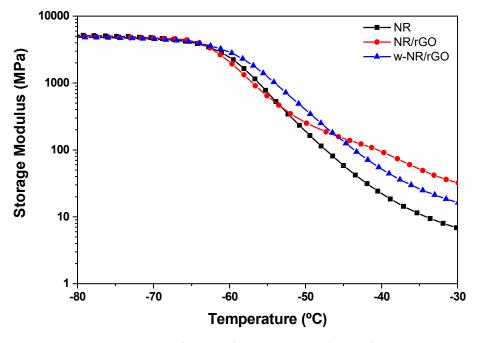


Figure 5. Storage modulus of NR, NR/rGO 4.0 wt.% and w-NR/rGO 4.0 wt.%.

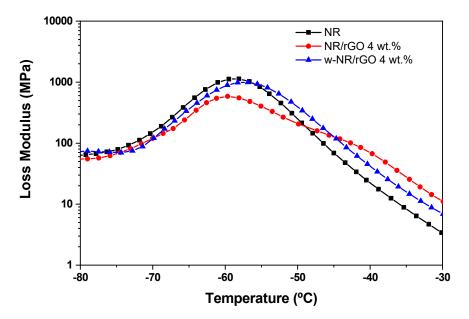


Figure 6. Loss modulus of NR, NR/rGO 4.0 wt.% and w-NR/rGO 4.0 wt.%.

4. Conclusions

Successful elimination of SDS surfactant from elastomer nanocomposites, based on NR/rGO, was demonstrated by using Raman spectroscopy. The elimination of this surfactant resulted in an improvement of the mechanical and electrical properties of the nanocomposites. In this respect, it was demonstrated that the percolation threshold decreased from 2.6 wt.% to 1.65 wt.% and the ultimate tensile strength slightly increased by the washing process. An important outcome of this research, as ascertained using dynamo-mechanical analysis, is that the presence of a surfactant impedes the free rotation of the natural rubber backbone.

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