

1 **QUINOA WET-MILLING: EFFECT OF STEEPING CONDITIONS ON STARCH**
2 **RECOVERY AND QUALITY**

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26 **Abstract**

27 Cereal starches play an important role in the food and non-food industries because of their
28 low cost, availability, and ability to impart a wide range of techno-functional properties. The
29 main objective of this research was to isolate starch, germ, protein, and fiber components
30 from quinoa by a wet-milling procedure. The effect of steeping time and temperature on
31 starch recovery and its quality was investigated. The quinoa steeping conditions, such as time
32 (1, 5, and 9 hours) and temperature (30, 40, and 50 °C), in SO₂ solution with lactic acid were
33 investigated using a 3² factorial design in order to optimize the starch separation and its
34 quality. The effect of steeping conditions on starch was evaluated in terms of whiteness,
35 protein, lipid, amylase, and damaged starch contents, as well as thermal and pasting
36 properties. Results showed how the different steeping times and temperatures affected the
37 fraction yields and starch recovery and its quality. Optimization of the wet-milling process
38 used in this study produced the highest starch recovery level and best starch quality after 6.5
39 hours of steeping at 30 °C. Experimental values were close to the predicted ones, with an
40 error below 2% for all attributes tested.

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48 **Keywords:** quinoa; wet-milling; steeping; starch recovery; starch quality; thermal and pasting
49 properties

50 **Abbreviations:**

51 ΔH_G , enthalpy of gelatinization; ΔH_R , enthalpy of retrogradation; a^* , redness to greenness; a_1
52 is the main effect of x_1 ; a_{12} is the mixed coefficient that represents the interactions between
53 factors; a_2 is the main effect of x_2 ; a_{ii} are the square coefficients that indicate if any of the
54 variables has a maximum or minimum in the experimental domain; b^* , yellowness to
55 blueness; CPV, final or cool paste viscosity; DSC, Differential Scanning Calorimetry; g,
56 grams; h, hour, HPV, hot paste viscosity; L^* , lightness; P_{temp} , pasting temperature; P_{time} , peak
57 time; PV, peak viscosity; rpm, revolutions per minute; RS-Q, adjusted square coefficient of
58 the fitting model; RVA, Rapid Visco Analyser; SW, leached solids in steepwater; T_c ,
59 conclusion temperature; T_o , onset temperature; T_p , peak temperature; WI, whiteness index;
60 WQF: whole quinoa flour; WW, solids in washing water; x_1 is the design factor steeping time;
61 x_2 is the design factor steeping temperature; Y_{calc} , data from the model; Y_{obs} , the experimental
62 data; ε is the difference between the experimental data and the model, the residual.

63 **1. Introduction**

64 The primary sources of carbohydrates for the global population are cereals and pseudocereals.
65 Pseudocereals are essentially starch crops; however, they may contain significant quantities of
66 protein and oil, and these constituents frequently determine their suitability for a specific end
67 use. In particular, quinoa is a pseudocereal native to South America, mainly from Peru,
68 Bolivia, Argentina, Colombia, Ecuador, and Chile, but in recent decades other countries such
69 as the United States, Canada, Italy, France, Spain, England, and Sweden have also become
70 producers (Bazile and Baudron, 2015). Structurally, quinoa is composed of three main parts:
71 the perisperm, the embryo or germ, and the pericarp or seed hull (Reguera and Haros, 2017).
72 The perisperm is the primary starch storage portion, the germ is the lipid storage portion, and
73 finally the hull, also called bran, consists mainly of cellulose and hemicellulose. The
74 physicochemical and functional properties of the main components of quinoa, starch, fiber,
75 and protein, are widely described in the literature (Koizol, 1992; Schoenlechner et al., 2010;
76 Kurek, et al., 2018). The objective of milling is to obtain intermediate products that can be
77 used subsequently in the manufacture of other products. Normally, milling schemes are
78 classified as dry- or wet-milling. In dry-milling the aim is to separate the anatomical part of
79 the grain to produce mainly flour, whereas the purpose of wet-milling is to separate the
80 chemical components of the grain, such as starch, proteins, fiber, and lipids, to obtain the
81 purest possible fraction of each component (Haros and Wronkowska, 2017). The main cereal
82 used in wet-milling is corn (maize). In conventional wet-milling, corn is steeped in an
83 aqueous solution containing sulfur dioxide (0.1–0.3%), an antimicrobial reducing agent,
84 which solubilizes and disperses the proteinaceous matrix that envelops and binds the starch
85 granules (Eckhoff and Tso, 1991; Calzetta-Resio et al., 2006). Modification of the structural
86 characteristics, and the physicochemical and functional properties of starch owing to steeping

87 and milling conditions has been reported in corn (Perez et al., 2001; 2003), wheat (Lorenz and
88 Kulp, 1978), and rice (Lee et al., 2004). Wet-milling is a more complex process than dry-
89 milling, and it is a source of a great variety of products. Although starch is the main product
90 of wet-milling, there are other subproducts that are used for technological and food purposes,
91 such as the fiber-rich and protein-rich fractions. The wet-milling of quinoa has not been
92 widely studied yet, especially the optimum parameters and the steeping conditions such as
93 time, temperature, pH, and stirring, among others. The steeping temperature is usually
94 between 28 and 55 °C, because it must be below gelatinization temperature. The steeping
95 time is conditioned by the type of grain, its morphology, and its size (Haros and
96 Wronkowska, 2017). Changes in these parameters are important in starch isolation and its
97 properties, determining its use (Haros and Wronkowska, 2017). Wright et al. (2002) used
98 steeping with sodium hydroxide for 12 h at room temperature to isolate starch from varieties
99 of sweet and bitter quinoa. Steffolani et al. (2013) and Jan et al. (2017a) isolated starch from
100 the flour of several varieties of quinoa by steeping with NaOH.

101 The main objective of this research was to develop and optimize a quinoa wet-milling
102 procedure for isolating the fractions of starch, proteins, and fiber at laboratory scale. The
103 effect of steeping time and temperature on starch recovery and its quality was also
104 investigated.

105

106 **2. Materials and methods**

107 ***2.1. Raw materials***

108 Commercial Bolivian seeds of quinoa (*Chenopodium quinoa*), Organic red Quinoa Real®
109 were purchased from ANAPQUI (La Paz, Bolivia).

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111 *2.2. Wet-milling procedure*

112 Previous studies, in which different steeping solution temperatures, times, and pHs were
113 evaluated, were used for reference purposes (Zheng et al., 1998; Calzetta-Resio et al., 2009;
114 Wronkowska and Haros, 2014). Quinoa seeds (50 g) were steeped in 500 mL of sufficient
115 sodium bisulfite to give a sulfur dioxide concentration of 0.25% at pH 5.0, adjusted with
116 lactic acid. The wet-milling tests were performed according to a 3² factorial design (Table 1),
117 and each experiment was conducted in duplicate. Two steeping variables – steeping time (1,
118 5, and 9 hours) and steeping temperature (30, 40, and 50 °C) – were assayed in a laboratory
119 fermenter (Biostat Bplus, Sartorius, Spain) with constant control of temperature, pH at 5.0
120 adjusted with lactic acid, and stirring at 300 rpm. The steeped quinoa was separated into
121 different fractions in two stages: a) the seeds were milled using a plate mill (Corona, Lambers
122 & Cia, Colombia) to separate the germ fraction by flotation in water. After separation, the
123 germ fraction was washed with ultrapure water (1 L) to remove the residual starch content
124 (Figure 1); b) the degerminated seed slurry obtained after the first milling was
125 scattered/homogenized with a disperser (PT 10/35 GT, Polytron, Lucerne, Switzerland). The
126 homogenization was performed with 200 mL of water at 15,000 rpm for 1 minute three times.
127 Then the homogenate was screened through two sieves (300 and 53 µm), where the hulls and
128 protein fractions were retained, respectively. The fractions were washed with ultrapure water
129 and the resulting suspension was centrifuged at 12,000 rpm for 15 min at 4 °C to obtain the
130 starch fraction. After centrifugation it was possible to separate the pure starch from the
131 tailings, the last were at the top of the pellet and were removed manually with a spatula
132 (Wronkowska and Haros, 2014). The fractions were dried in a forced-air oven at 40 °C
133 overnight, and aliquots of the steepwater (SW) and washing water (WW) were dried at 70 °C

134 in a forced-air oven to determine the soluble and suspended solids (total solids). All fractions
135 were stored in sealed plastic containers until their analysis in a chamber at 14 °C.

136 The yield of each fraction, expressed as a percentage, was calculated as the ratio of the totally
137 dried isolated fraction to the initial amount of dried quinoa, as:

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$$139 \quad \text{Yield (\%)} = \frac{\text{dry weight of separated fraction}}{\text{initial dry weight of grain}} \times 100 \quad (1)$$

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141 The starch recovery was calculated as the ratio of the dry weight of the isolated starch to the
142 dry weight of starch in grain:

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$$144 \quad \text{Starch recovery(\%)} = \frac{\text{dry weight of isolated starch}}{\text{dry weight of starch in grain}} \times 100 \quad (2)$$

145

146 **2.3. Physicochemical starch characterization**

147 Moisture content was determined following the official assay procedure (Method 925.09,
148 AOAC, 1996). Starch content was measured by the total starch assay procedure (AOAC,
149 1996). The protein and lipid contents were determined by the Dumas combustion method
150 (Nx5.7) according to ISO/TS 16634-2 (2016) and the Soxhlet technique (Method 30-20,
151 AACC 1995) with petroleum ether under reflux conditions, respectively.

152 The amylose and amylopectin contents were determined using a commercial assay kit
153 (Megazyme International Ireland Ltd., Bray, Co. Wicklow, Ireland) based on the
154 Concanavalin-A method developed by Yun and Matheson (1990). The instrumental color of
155 the starchy fraction was measured with a digital colorimeter (Chroma Meter CR-400, Konika
156 Minolta Sensing, Japan). The parameters determined were L* (lightness), a* (redness to

157 greenness), and b* (yellowness to blueness), and the whiteness index (WI) was calculated by
158 the following equation: $WI=100-((100-L)^2+a^2+b^2)^{0.5}$. All the analyses were done in triplicate.

159

160 ***2.4. Determination of quinoa starch thermal properties***

161 A differential scanning calorimeter (DSC-7, PerkinElmer, USA) was used to measure the
162 thermal properties of the raw materials and starch fractions, and the amylopectin
163 retrogradation. The DSC was calibrated with indium (enthalpy of fusion 28.4 J/g, melting
164 point 156.4 °C). Samples were weighed into DSC pans (LVC 0319-0218, PerkinElmer), and
165 ultrapure water was added to obtain a water:flour ratio of 3:1 in order to ensure complete
166 gelatinization. After sealing, the pans were left for a few hours to equilibrate the humidity,
167 and then they were scanned at a rate of 10 °C/min from 20 to 130 °C. Subsequently, the pans
168 were stored at 4 °C for 2 days, and then heated again in the calorimeter from 20 to 130 °C at
169 10 °C/min to analyze amylopectin retrogradation. An empty pan (air) was used as a reference,
170 and three replicates of each sample were analyzed. Thermal transitions of starch were defined
171 in terms of onset temperature (T_o), peak (T_p), conclusion temperature (T_c), and enthalpy of
172 gelatinization and amylopectin retrogradation (ΔH_G and ΔH_R , respectively), expressed in J/g
173 of starch (Haros et al., 2004).

174

175 ***2.5. Pasting properties of quinoa starch***

176 The pasting properties of the starch fractions were measured using a Rapid Visco Analyser
177 (RVA-4; Newport Scientific, Warriewood, Australia) according to AACC Method 76-21
178 (1995). Distilled water (25 mL) was added to 3.0 or 3.5 g of sample placed in the aluminum
179 RVA canister. The suspensions were stirred thoroughly at 160 rpm. The temperature was first
180 maintained at 50 °C for 1 min and then raised to 95 °C at a rate of 12 °C/min, held at 95 °C

181 for 2.5 min, cooled to 50 °C at the same rate, and finally held at 50 °C for 2 min. Pasting
182 parameters evaluated included: pasting temperature (P_{temp}), peak viscosity (PV), peak time
183 (P_{time}), hot paste viscosity (HPV), final or cool paste viscosity (CPV), breakdown (PV-HPV),
184 and setback (CPV-HPV). The experiments were conducted in triplicate.

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186 **2.6. Factorial design and statistical analysis**

187 In order to study the effect of steeping conditions on starch recovery and quality, a factorial
188 design was used. The independent factors studied were time (1, 5, and 9 hours) and
189 temperature (30, 40, and 50 °C) at three levels. The run conditions of a 3^2 factorial design are
190 shown in Table 1 in terms of experimental conditions and coded values. The design makes it
191 possible to approximate the experimental data (Y_{obs}) with a response surface model expressed
192 in coded values:

193

$$194 \quad Y_{obs} = a_0 + a_1x_1 + a_2x_2 + a_{12}x_1x_2 + a_{11}x_1^2 + a_{22}x_2^2 + \varepsilon \quad (3)$$

195

196 In Equation 3, x_1 is the design factor steeping time, and x_2 is the steeping temperature. The
197 coefficients a_1 and a_2 are the main effects of x_1 and x_2 , respectively. The square coefficients
198 (a_{ii}) indicate if any of the variables has a maximum or minimum in the experimental domain,
199 whereas the mixed coefficients (a_{12}) represent the interactions between factors. The difference
200 between the experimental data (Y_{obs}) and the model (Y_{calc}) gives the residual (ε). For each
201 response the RS-Q was calculated, which is the fraction of variation of the response explained
202 by the model.

203

204 **2.7. Statistical analysis**

205 The multivariate analyses (stepwise regressions, multiple way analysis of variance, and
206 correlation matrix) of the yields of quinoa fractions after wet-milling, and the
207 physicochemical, thermal, and pasting properties of the starch fractions were performed using
208 the Statgraphics[®] software package (Statistical Graphics Corporation, Virginia, Washington,
209 DC, USA).

210

211 **3. Results and discussion**

212 ***3.1. Effect of steeping condition on yields***

213 The composition of raw material used in this investigation was : moisture, 10.68±0.02; starch,
214 67±3; protein, 12.8±1.0; lipid, 7.3±0.6, and ash contents, 2.32±0.04 g/100 g in dry matter
215 (d.m.).

216 The fraction yields obtained by quinoa wet-milling were: 7.1–13.3% of germ, 9.1–14.6% of
217 fiber, 0.9–2.6% of protein, 54.9–58.5% of starch, 5.2–17.9% of total solids in steepwater, and
218 4.1–10.8% in washing water, expressed in dry matter. The starch yields in the current
219 investigation were slightly higher than those reported by Wright et al. (2002), and much
220 higher than those obtained by Jan et al. (2017a) using different steeping conditions and wet-
221 milling procedure. Wright et al. (2002) performed the steeping step in 0.30% NaOH at room
222 temperature for 12 h. In the case of Jan et al. (2017b), quinoa seeds were steeped in alkali
223 solution (0.20, 0.25, and 0.30% NaOH) at ~4 °C for 24 h.

224 The analytical data obtained from the factorial design for the yields of quinoa fractions
225 obtained by wet-milling were fitted to multiple regression equations using three levels of two
226 independent factors (Table 2) in order to estimate the dependence of yields (Eq. 3). The
227 results obtained showed that the steeping time factor significantly affected the yields of the
228 quinoa fractions ($p<0.01$). In general, when the steeping time increased, the germ yield and

229 SW solids increased significantly (by 19–46% and 76–93%, respectively), whereas the other
230 yields decreased significantly (fiber, protein, starch, and WW fractions). The total solids (SW)
231 leached in the steepwater increased significantly with steeping time at the expense of
232 degradation of grain components during this step (Perez et al., 2003).

233 The steeping temperature individually promoted the largest increase in the germ yield (from
234 7.1-11.4 % (at 30°C) to 10.5-12.8 % (at 50°C)) and in the SW solid fraction (from 5.2-13.0 %
235 (at 30°C) to 8.1-17.9 % (at 50°C)).

236 As a global tendency, the starch yields and recoveries decreased with the increase in steeping
237 temperature, as indicated by the a_2 coefficient (Tables 2 and 3, respectively). In contrast, the
238 steeping time, as a single independent variable, did not show any significant effect on the
239 starch yields/recoveries. However, it was reported that corn starch yields increased as the
240 steeping time increased (Perez et al., 2001). These discrepancies could be due to the ability of
241 sulfur dioxide/lactic acid in the steepwater to disperse the protein matrix that envelopes the
242 starch granules. This fact is less significant in quinoa than in corn, which the grain is harder
243 and the starch is strongly linked protein matrix (Dailey, 2002; Perez et al., 2003; Wronkowska
244 and Haros, 2014). In addition, there was a significant effect derived from the interaction
245 between steeping time and temperature (a_{12} , Tables 2 and 3). On the other hand, as a result of
246 the factorial design, the starch yield/recovery presented a maximum value in the domain
247 studied, as represented by the negative quadratic coefficient of steeping time a_{11} (Tables 2 and
248 3, respectively).

249 The fiber yields also presented a significant interaction coefficient between the two factors
250 studied (Table 2). The quadratic coefficient of the steeping time factor (a_{11}) was also
251 significant for the fiber and protein yields, in both cases indicating a minimum value of these

252 fractions within the domain studied (Table 2). On the other hand, the quadratic coefficient of
253 the steeping temperature factor (a_{22}) was non-significant for any of the by-products.

254 It is observed that even though the increase of steeping time causes more solids to leach into
255 the steep water, such an increase was particularly pronounced at 50°C of steeping. It was
256 reported that when lactic acid was present in the steepwater an increment of the proteolytic
257 activity resulting from the action of that chemical (Perez et al., 2001). One of the main
258 contribution to the increase of leached solids could be due to increased solubility of protein by
259 the action of lactic acid, so the protein fraction decreased significantly with the steeping time
260 (a_1 : -0.497). On the other hand, when the steeping time increased the germ fraction
261 augmented and the fiber fraction decreased probably due to the better separation of embryo
262 and higher soluble fiber lost, respectively.

263

264 ***3.2. Starch recovery and physicochemical characterization***

265 Results of starch recovery and physicochemical characterization in terms of factorial design
266 coefficients are shown in Table 3. In general, as the steeping temperature increased the starch
267 recoveries decreased, whereas the steeping time showing a maximum in this parameter (Table
268 3). However, it is important to take into account that there was also a significant interaction
269 between the two factors, as mentioned earlier. The absolute values of the starch recoveries
270 were within the range 81.9 ± 0.1 – $87.2 \pm 0.7\%$ in dry matter. There are only a few investigations
271 on quinoa wet-milling and the recoveries were not reported. Nevertheless, the results of the
272 current investigation could be compared with previous data for cereals and/or other
273 pseudocereals. The starch recovery/efficiency in corn was around 85.1% d.m. (Perez et al.,
274 2003), in amaranth 67.7% d.m. (Calzetta-Resio et al., 2009), in buckwheat 64.6% d.m.

275 (Wronkowska and Haros, 2014), and in rice 69.6% (Loubes et al., 2016), at the same order of
276 magnitude as the current investigation.

277 With regard to the protein and damaged starch contents in the starch fraction, neither steeping
278 time nor steeping temperature affected them significantly (Table 3). The results varied in the
279 range 1.56 ± 0.02 – $1.9\pm 0.8\%$ protein d.m. and 5.5 ± 0.1 – $7.5\pm 0.2\%$ damaged starch d.m.

280 It was also observed that the amylose content of the starch decreased significantly only with
281 the linear factor steeping time. This could be due to the higher hydrolysis of amylose during
282 this step, as evidenced by the significantly higher amount of total solids in steepwater after 9
283 hours of steeping (from 5.2–8.1 to 13.0–17.9% d.m., for 1 and 9 h, respectively). On the other
284 hand, the starch whiteness index quality parameter was significantly affected by the linear
285 steeping temperature factor (Table 3), which decreased slightly with the increase in
286 temperature (from 91 to 89% for 30 °C and 50 °C, respectively).

287 The starch physicochemical properties of quinoa obtained under the various steeping
288 conditions by wet-milling were similar to the results reported by Steffolani et al. (2013), and
289 slightly higher than those reported by Jan et al. (2017a, 2017b). In the current study the non-
290 detection of lipids owing to efficient separation of the germ during the wet-milling procedure
291 was a valuable result from the point of view of starch quality and in comparison with other
292 investigations (Wright et al., 2002; Steffolani et al., 2013; Jan et al., 2017a).

293

294 ***3.3. Effect of steeping conditions on thermal properties***

295 The DSC analysis of quinoa starch revealed how the steeping time and steeping temperature
296 affected the thermal properties. Factorial design showed that the initial and peak temperatures
297 of both gelatinization and retrogradation were significantly affected by both steeping factors.
298 In general, they were higher when the steeping time and temperature increased (T_{oG} : from

299 51.2±0.1 °C to 55.4±0.5 °C; T_{pG}: from 58.6±0.1 °C to 61.1±0.1 °C; T_{oR}: from 35.6±0.2 °C to
300 40.0±0.5 °C; T_{pR}: 45.5±0.1 °C to 47.8±0.1 °C), whereas the conclusion temperatures were not
301 affected significantly (T_{cG}: 68.2±0.3–70.1±0.2 and 55.6±0.5–56.8±0.5 °C). In addition, the
302 factors showed a significant interaction in T_o and T_p of gelatinization, as well as a significant
303 effect on the quadratic terms, which indicated the presence of a maximum in T_o (steeping time
304 factor, *a₁₁*) and a minimum in T_o and T_p (steeping temperature factor, *a₂₂*) in the response
305 surface, respectively.

306 The increase in T_o and T_p, with a narrower gelatinization temperature range, suggests a partial
307 annealing effect. This behavior was also observed in corn starch (Perez et al., 2001, 2003), in
308 wheat starch (Lorenz and Kulp, 1978), and in rice starch (Lee et al., 2004) with an increase in
309 steeping time. Annealing is defined as the heating of starch in excess water at
310 subgelatinization temperatures, which are the conditions during steeping (Perez et al., 2001;
311 Falade and Ayetigbo, 2015). It may provoke partial melting of some crystals and realignment
312 of starch chains in the amorphous regions, giving rise to more ordered crystals with higher
313 melting points (Perez et al., 2001).

314 The steeping conditions did not significantly affect the enthalpy of gelatinization, as was also
315 observed previously in corn wet-milling and rice wet-milling by other researchers (Perez et
316 al., 2001; Lee et al., 2004). It was reported that annealing has no effect on ΔH_G (Knutson,
317 1990), but it was also stated that the more crystalline structure are before annealing, the less
318 they can be enhanced by the annealing process (Alvani et al., 2012).

319 In the current investigation, the enthalpies of gelatinization and retrogradation were in the
320 range of 12.4±0.3–13.5±0.1 J/g of starch for ΔH_G and 1.2±0.2–1.7±0.2 J/g of starch for ΔH_R,
321 respectively. The results of enthalpy of gelatinization are in agreement with those reported by

322 Wright et al. (2002) for starches isolated from several varieties of quinoa. On the other hand,
323 Steffolani et al. (2013) reported slightly higher values in quinoa and kañiwa starches.
324 Results for enthalpy of retrogradation were higher, by ~26%, than those reported by
325 Steffolani et al. (2013) after 14 days of storage at 4 °C. Srichuwong et al. (2017) reported
326 retrogradation temperatures in accordance with our results (36.2–61.7 °C) after 6 days of
327 storage at 4 °C. However, the enthalpy of retrogradation was higher (4.2 J/g starch) than in
328 this study, probably owing to the longer storage time in their case.

329

330 ***3.4. Influence of steeping conditions on quinoa starch pasting properties***

331 The values of the pasting property parameters were: from 3898 to 3064 cP for PV, from 3430
332 to 2231 cP for HPV, from 4340 to 3557 cP for CPV, from 7.00 to 6.72 min for P_{time} , and from
333 68.44 to 64.50 °C for P_{temp} . These results are in agreement with those reported by Wu et al.
334 (2017) for starch from several varieties of quinoa. Steffolani et al. (2013) observed similar
335 values, with the exception of P_{time} (5.17–4.97 min) and P_{temp} (62.7 °C), which were slightly
336 lower than our results. In general, variation of steeping temperature did not modify the
337 pasting properties, and no significant differences were found in the RVA parameters of
338 quinoa starch with the exception of the pasting temperature (P_{temp}). This parameter increased
339 slightly with the increase in temperature and presented a maximum (Table 3). It was observed
340 that the linear effect of steeping time significantly affected the coefficients of the PV, HPV,
341 and CPV parameters, causing a decrease in them when the time increased. In contrast, setback
342 increased significantly as the steeping time increased. However, all these tendencies seemed
343 to be significant for the first 5 hours of steeping, whereas longer steeping times did not seem
344 to modify the viscosity profile (Figure 3). The PV decreased by about 11–14% between 1
345 hour of steeping and 9 hours of steeping. This parameter indicates the starch water-binding

346 capacity and gives an indication of the viscous load. A drop in its value is usually brought
347 about by partial hydrolysis (Haros et al., 2004; 2006). The steeping chemicals, such as SO₂
348 and lactic acid, could hydrolyze the starch and reduce the pasting viscosities because they
349 diffuse into the starch granules during their hydration and swelling (Shandera and Jackson,
350 1996; Haros et al., 2006). After reaching PV the swollen starch granules are easily broken and
351 disintegrated by stirring, so the viscosity decreases to a minimum, the hot paste viscosity
352 (HPV). During the hold period at 95 °C and mechanical shear stress, the starch granules
353 disrupt and amylose molecules leach out into the solution (Haros et al., 2006). The HPV
354 dropped significantly during the first hour of steeping at all the temperatures studied. After
355 the cycle of heating and cooling a reassociation between amylose molecules occurs. If the
356 concentration is sufficient they form a gel and the viscosity increases up to a final viscosity
357 (CPV) which involves the retrogradation phenomenon. In the current investigation CPV also
358 dropped significantly in the starch fraction after steeping, probably owing to the partial loss of
359 amylose. As described above, the amylose content of starch decreased significantly with the
360 steeping time factor (Table 3), from 23.1±0.8–26.5±0.4% to 19.2±0.2–24.0±0.2% for 1 hour
361 and 9 hours of steeping, respectively, which could explain the changes observed in pasting
362 properties (Figure 3).

363 The values of the pasting property parameters were: from 3898 to 3064 cP for PV, from 3430
364 to 2231 cP for HPV, from 4340 to 3557 cP for CPV, from 7.00 to 6.72 min for P_{time}, and from
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367 values, with the exception of P_{time} (5.17–4.97 min) and P_{temp} (62.7 °C), which were slightly
368 lower than our results.

369

370 **3.5. Optimization of steeping conditions**

371 The calculation of the optimum experimental conditions to be used was performed for the
372 recovery parameter, taking into account the starch physicochemical properties of quinoa in
373 terms of protein content, damaged starch, and whiteness index. The effects of time (x_1) and
374 temperature (x_2) on starch recovery were satisfactorily simulated by Equation (3). The
375 maximum expected starch recovery (85.7%) occurred at 6.5 h of steeping time at 30 °C.
376 Expected responses for steeping time and temperature factors in comparison with values
377 reported by other authors are shown in Table 4. In general, the expected values were higher
378 than those reported in other studies. This expected response was corroborated experimentally.
379 The expected responses were tested, and the results were: $86.7 \pm 1.6\%$ (d.m.) for starch
380 recovery, $62.3 \pm 0.8\%$ for starch yield, $1.74 \pm 0.05\%$ of protein, and $91.8 \pm 0.08\%$ of whiteness.
381 The differences between the experimental and expected responses presented a deviation of
382 only 2%.

383

384 **4. Conclusions**

385 The quinoa wet-milling process proved to be a potential procedure for obtaining various
386 valuable components of quinoa grains. The factorial design showed that the variables steeping
387 time and temperature affect the parameters significantly, increasing or decreasing their values,
388 depending on the parameter analyzed. The wet-milling process developed in this study
389 achieved a high level of starch recovery from quinoa. Maximum response values were
390 obtained when the steeping time was set at 6.5 hours and the steeping temperature at 30 °C.
391 It is still necessary to study quinoa starch more deeply, because its propitious properties may
392 have application potential in areas such as novel food additives, fat replacement,
393 pharmaceuticals, cosmetics, papermaking, and textiles. Finally, the economic cost of steeping

394 operating conditions and the starch quality/recovery obtained by using a wet-milling
395 procedure should be evaluated in order to find the most suitable conditions at industrial level.

396

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402

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511 **Figure captions**

512

513 **Figure 1.** Laboratory Quinoa Wet-Milling

514

515 **Figure 2.** Influence of interaction between steeping time (x_1) and steeping temperature (x_2) on yields
516 of **A.** Germ, **B.** Fiber, **C.** Protein, **D.** Starch.

517

518 **Figure 3.** Effect of steeping conditions on pasting profile of starch obtained by wet-milling. **A.** 30 °C;
519 **B.** 40 °C; **C.** 50 °C; — 1 h; — — 5 h; 9 h; — quinoa whole flour.

520

521 **Table 1.** Factorial design for sampling

522

Run	Name	Steeping Conditions		Coded Value	
		time, h	Temperature, °C	time, x_1	Temperature, x_2
1	WM1-30	1	30	-1	-1
2	WM1-40	1	40	-1	0
3	WM1-50	1	50	-1	1
4	WM5-30	5	30	0	-1
5	WM5-40	5	40	0	0
6	WM5-50	5	50	0	1
7	WM9-30	9	30	1	-1
8	WM-9-40	9	40	1	0
9	WM9-50	9	50	1	1

523

524 **Table 2.** Factorial design coefficients of yield of by-products of quinoa wet-milling

525

Coefficient	Constant	Linear		Quadratic		Interaction	R-SQ
	a_0	a_1	a_2	a_{11}	a_{22}	a_{12}	
Germ	11.866	1.763**	1**				0.83
Fiber	9.444	-1.682**		1.479**		0.82**	0.88
Protein	1.118	-0.497**		0.472*			0.79
Starch	57.636		-0.789*	-1.689**		-1.055*	0.72
SW	13.787	4.565**	2.302**				0.94
WW	6.220	-2.152**					0.70

526

527 0.05 (*) and 0.01 (**) indicate statistically significant at the 95 and 99% confidence levels, respectively.

528 SW: leached solids in steepwater, % in dry matter.

529 WW: solids in washing water, % in dry matter.

530 a_1 and a_2 are the coefficients of the main single effects of x_1 and x_2 , respectively (x_1 is the design factor steeping

531 time, x_2 is the steeping temperature). The square coefficients (a_{ii}) indicate if any of the variables has a maximum

532 or minimum in the experimental domain, whereas the mixed coefficients (a_{ij}) represent the interactions between

533 factors. R-SQ: adjusted square coefficient of the fitting model.

534 **Table 3.** Factorial design coefficients of physicochemical, thermal, and pasting properties of quinoa
 535 starch isolated by wet-milling
 536

Coefficient	Constant a_0	Linear		Quadratic		Interaction a_{12}	R-SQ
		a_1	a_2	a_{11}	a_{22}		
Physicochemical characteristics							
Recovery, % d.m.	85.898		-1.176*	-2.514**		-1.574**	0.72
Protein, % d.m.	1.674						0.65
Damage, % d.m.	4.481						0.36
Whiteness Index	91.788		-0.703*				0.74
Amylose, % d.m.	22.937	-2.232**					0.66
Thermal Properties							
Gelatinization							
T _o , °C	51.428	0.558**	1.573**	-0.74*	1.67**	0.957**	0.94
T _p , °C	58.656		0.632**		1.594**	0.796**	0.85
T _c , °C	68.719	-0.513**					0.71
ΔH _G , J/g of starch	13.132						0.45
Retrogradation							
T _o , °C	38.161	1.411**	0.694*				0.79
T _p , °C	47.078	0.822**	0.432*				0.81
T _c , °C	55.749						0.21
ΔH _R , J/g of starch	1.179						0.32
Pasting							
P _{temp} , °C	66.396		0.949*	-1.428*			0.64
P _{time} , min	6.915						0.29
PV, cP	3333.39	-230.25**					0.67
HPV, cP	2669.5	-296.0**					0.68
CPV, cP	3845.83	-181.67*					0.60
Breakdown, cP	664.11						0.55
Setback, cP	1170.61	105.0*		-139.17*			0.64

537
 538 0.05 (*) and 0.01 (**) indicate statistically significant at the 95 and 99% confidence levels, respectively.
 539 DSC, Differential Scanning Calorimetry; T_o, onset temperature; T_p, peak temperature, T_c, conclusion
 540 temperature; ΔH_G, enthalpy of gelatinization, J/g in d.m.; ΔH_R enthalpy of retrogradation, J/g in d.m.
 541 RVA: Rapid Visco Analyser; P_{temp}, Pasting temperature; P_{time}, Peak time; PV, Peak viscosity; HPV, hot paste
 542 viscosity; CPV, final or cool paste viscosity; Breakdown: PV-HPV; Setback, CPV – HPV; cP, centipoise; d.m.,
 543 dry matter. a_1 and a_2 are the coefficients of the main single effects of x_1 and x_2 , respectively (x_1 is the design
 544 factor steeping time, x_2 is the steeping temperature). The square coefficients (a_{ii}) indicate if any of the variables
 545 has a maximum or minimum in the experimental domain, whereas the mixed coefficients (a_{ij}) represent the
 546 interactions between factors. R-SQ: adjusted square coefficient of the fitting model.
 547

548 **Table 4.** Expected yield, recovery, and physicochemical composition of quinoa starch fractions, and
 549 comparison with other investigations
 550

Parameter of Starch Fraction	Unit s	Current Investigation^a	Jan et al., 2017a,b	Steffolani et al., 2013	Wright et al., 2002
Yield	%.	61.89	48.52	NR	53.3
Recovery	%	85.68	NR	NR	NR
Protein	%	1.78	0.95	1.09	0.46
Lipids	%	ND	0.40	1.94	NR
Whiteness Index	%	91.45	NR	NR	NR
Amylose	%	23.9	12.1	17.4	20.6
Damaged Starch	%	4.65	NR	NR	NR

551
 552 ^aexpressed in dry matter.
 553 ND: Not detected; NR: Not reported.
 554 Steeping conditions: Jan et al. (2017a, 2017b): 0.25% NaOH, 24 h; Steffolani et al. (2013): 0.25% NaOH, 12 h;
 555 Wright et al. (2002): 0.30% NaOH, 12 h.
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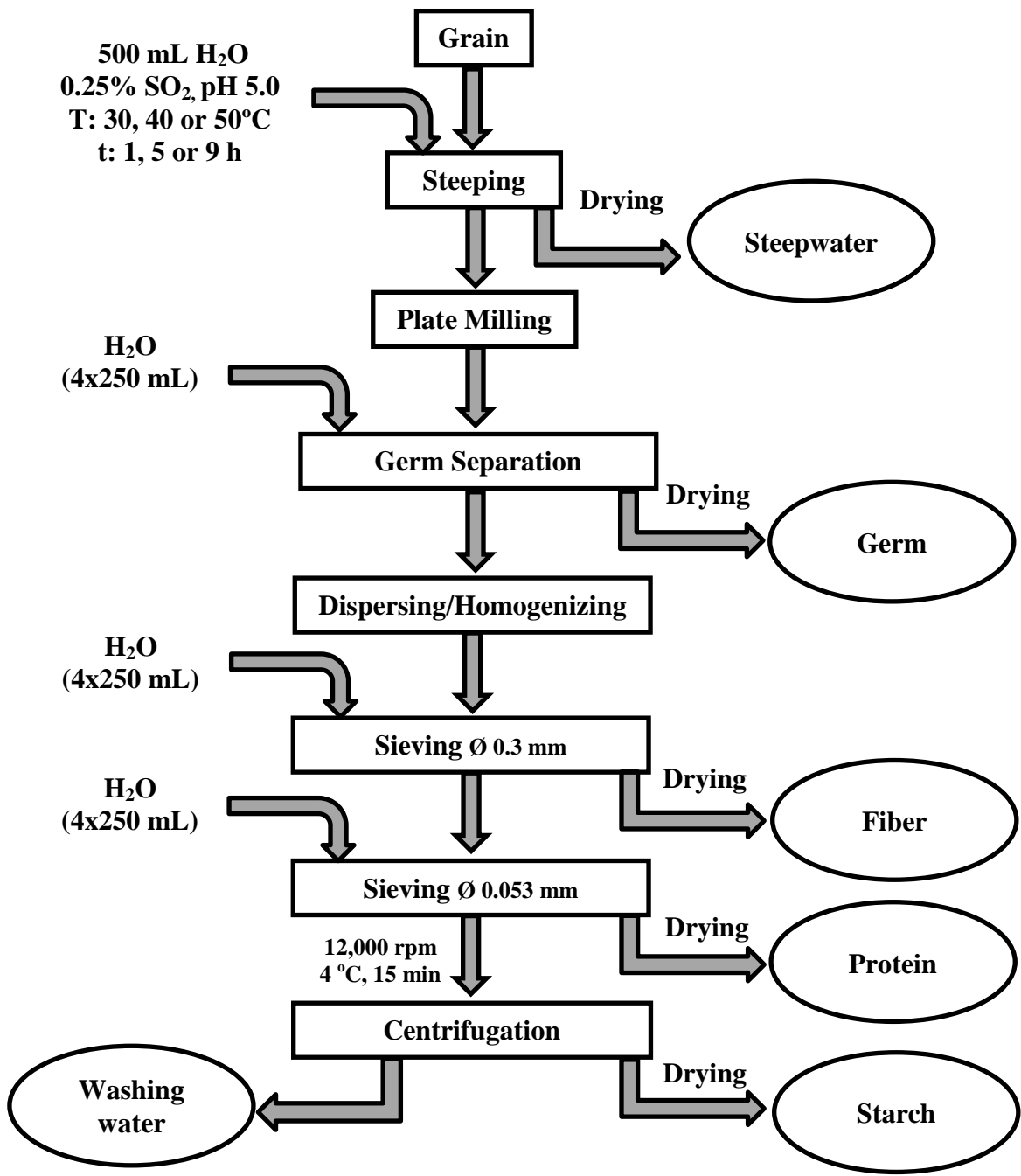


Figure 1

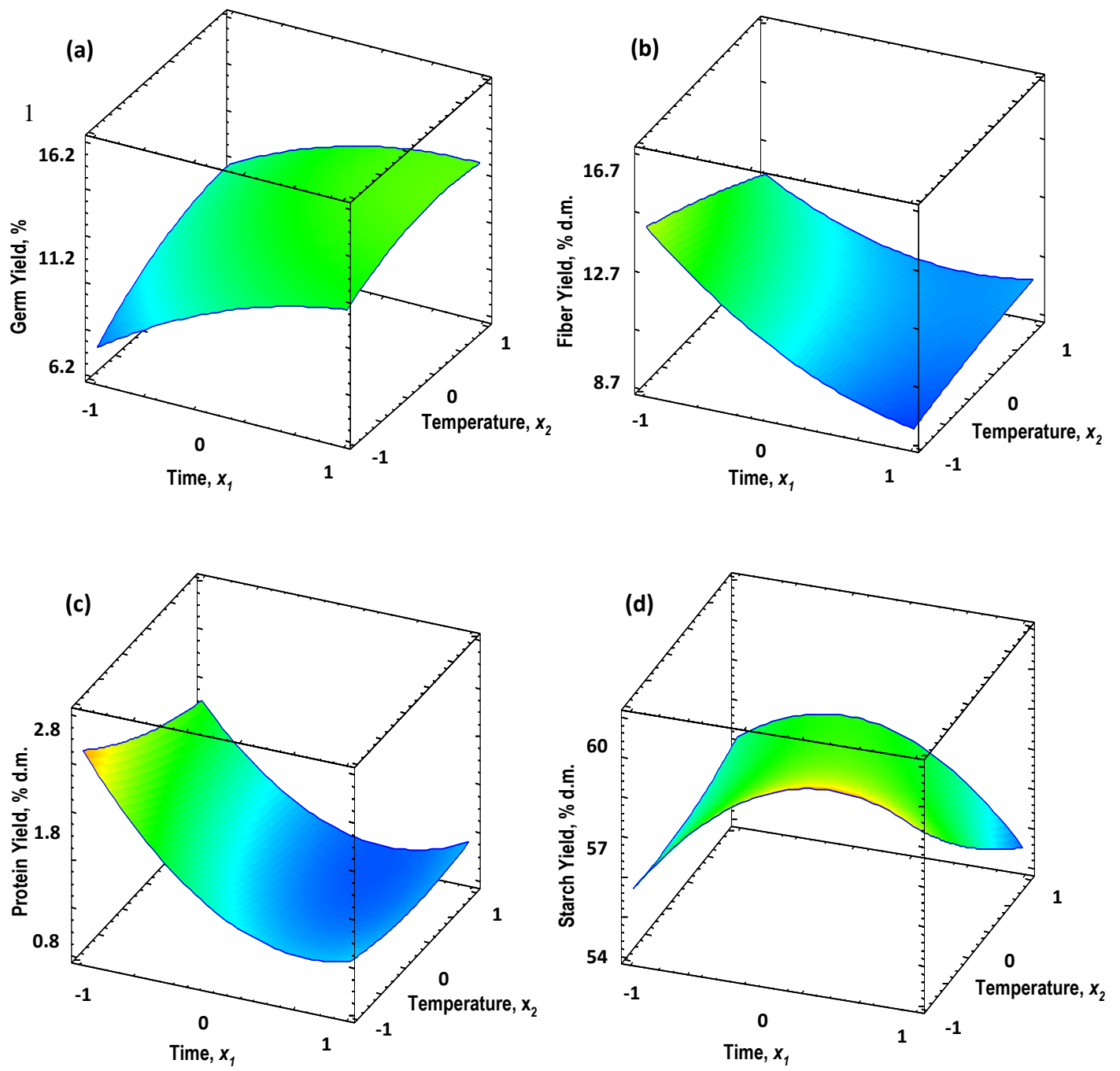


Figure 2

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