

1                    **Comparison of Solvent Extraction and Extraction Chromatography Resin**  
2                    **Techniques for Uranium Isotopic Characterization in High-Level Radioactive**  
3                    **Waste and Barrier Materials**

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16

17                    **Abstract**

18                    The development of Deep Geological Repositories (DGP) to the storage of high-level  
19                    radioactive waste (HLRW) is mainly focused in systems of multiple barriers based on the  
20                    use of clays, and particularly bentonites, as natural and engineered barriers in nuclear waste  
21                    isolation due to their remarkable properties.

22                    Due to the fact that uranium is the major component of HLRW, it is required to go in  
23                    depth in the analysis of the chemistry of the reaction of this element within bentonites. The

24 determination of uranium under the conditions of HLRW, including the analysis of silicate  
25 matrices before and after the uranium-bentonite reaction, was investigated. The  
26 performances of a state-of-the-art and widespread radiochemical method based on  
27 chromatographic UTEVA resins, and a well-known and traditional method based on  
28 solvent extraction with tri-n-butyl phosphate (TBP), for the analysis of uranium and  
29 thorium isotopes in solid matrices with high concentrations of uranium were analysed in  
30 detail.

31 In the development of this comparison, both radiochemical approaches have an overall  
32 excellent performance in order to analyse uranium concentration in HLRW samples.  
33 However, due to the high uranium concentration in the samples, the chromatographic resin  
34 is not able to avoid completely the uranium contamination in the thorium fraction.

### 35 **Keywords**

36 high-level radioactive waste; UTEVA; TBP; uranium; thorium

### 37 **1. Introduction**

38 Many researchers are devoted to the development of Deep Geological Repositories (DGP)  
39 to the storage of high-level radioactive waste (HLRW). Mainly the selected solution is  
40 based on a system of multiple barriers. Most of security of the disposal relies on an  
41 engineered barrier. Clays are ideal materials for natural and engineered barriers for nuclear  
42 waste isolation due to their high sorption capacity, low permeability, and swelling  
43 capability. In experimental conditions, it is found that the radioactive wastes are  
44 immobilised and their diffusion prevented through physical-chemical mechanism with a  
45 clay barrier, such as precipitation, adsorption or a chemical reaction including the  
46 formation of secondary stable mineral phases. At present, bentonite is established as the  
47 most appropriate clay to form the engineered barrier in the DGP (Kaufhold et al., 2015).

48 Previous papers have analysed the capacity of retention and the kinetics reaction properties  
49 of bentonites in relation to several radionuclides such as  $^{152}\text{Eu}$  (Alba et al., 2011; Mrabet

50 et al., 2014; Villa-Alfageme et al., 2014), additionally trivalent simulators of actinides have  
51 been used to study their potential retention capacity of HLRW by bentonites (Alba et al.,  
52 2009; Alba and Chaín, 2007). Determination of radionuclides in HLRW is important for  
53 nuclear waste management. Because uranium is the major component of HLRW, it is  
54 required to go in depth in the analysis of the chemistry of this element within bentonites  
55 and other clays and for this, specific radiochemical methods must be developed.  
56 Additionally, uranium undergoes a decay chain containing several radioactive isotopes,  
57 such as thorium and polonium, that have also to be analysed within HLRW.

58 A complete control of the geochemical behaviour of uranium under the specific conditions  
59 created by HLRW includes the analysis of silicate matrices before and after the uranium-  
60 bentonite reaction. Because this step is crucial when performing a complete study of the  
61 reaction properties of the system uranium-bentonite. It is then key to develop suitable  
62 methods for this kind of determinations.

63 Among the methods proposed in the literature to determine uranium in several matrices,  
64 the most recent ones are focused on behaviour of selected fission products and actinides on  
65 UTEVA resin (Skinner and Knight, 2016), purification of uranium using *n*-tri butyl  
66 phosphate (TBP) as extractant and *n*-decanol as phase modifier (Pradeep and Biswas,  
67 2017), extraction of uranium from simulated highly active feed in a micromixer-settler with  
68 30% TBP and 36% TiAP solvents (Kumar et al., 2017), diluted salts by TBP and dialkyl  
69 amides (Ansari et al., 2016), or uranyl selective polymeric membrane electrodes (Badr et  
70 al., 2014). However, it is not analysed the suitability and the sensitivity of currently  
71 available radiochemical methods when uranium must be quantified in complex matrices  
72 related to HLRW.

73 For this reason, in this study the performances of one state-of-the-art and widespread  
74 radiochemical method for the analysis of uranium (and additionally thorium and polonium)  
75 isotopes in solid matrices (Mas et al., 2012) was analysed in detail when it is applied to the  
76 measurement of matrices with high concentrations of uranium. This method combines a  
77 sequential separation of polonium-thorium-uranium using chromatographic UTEVA  
78 (Triskem Int.) resins and alpha spectrometry as radiometric measurement method.

79 Additionally, a well-known and traditional method was used to compare the performance  
80 of the UTEVA resins. In that case, uranium and thorium were extracted using tri-n-butyl  
81 phosphate (TBP) as solvent extraction method, combined with AG1-X8 ion-exchange resin  
82 (Villa et al., 2011). This method has the main drawback that is time consuming, but is a  
83 routine and robust method to extract uranium, thorium and plutonium as part of the nuclear  
84 reprocessing process (Dey and Bansal, 2006).

85 The analysed matrices were uranyl nitrates, and bentonites after a hydrothermal treatment  
86 with uranyl nitrate. The main objective of this paper is to analyse the performance of the  
87 UTEVA method to be used as a routine method to evaluate uranium, and additionally  
88 thorium and polonium, in HLRW samples, where high uranium concentrations are  
89 expected.

## 90 **2. Experimental**

### 91 *2.1. Sample preparation*

92 In the comparative study between both radiochemical methods, a simulated HLW material  
93 was prepared by using two different matrices: uranyl nitrate 6-hydrate  $\text{UO}_2(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$   
94 (supplied by Panreac) and FEBEX bentonite (from the Cortijo de Archidona deposit,  
95 Almería, Spain) (Enresa, 2000). Eight aliquots of this simulated HLW material were  
96 prepared and arranged in two groups.

97 In a first group, four aliquots of 0.0048 g of pure uranyl (0.0022 g of uranium) were  
98 analysed.  $^{232}\text{U}$ ,  $^{229}\text{Th}$  and  $^{209}\text{Po}$  were initially added to the aliquots as internal tracers. The  
99 first two aliquots (U-UTEVA-1 and U-UTEVA-2) were analysed following the UTEVA  
100 procedure later described, and only the second two aliquots (U-TBP-1 and U-TBP-2) were  
101 analysed following the TBP extraction procedure because it is a well-established method  
102 that we use as standard method of analysis.

103 In a second group, a total of four aliquots were prepared to check the performance of  
104 UTEVA chromatographic resin.  $^{232}\text{U}$  was added as internal tracer to those four aliquots in  
105 order to quantify uranium separation through UTEVA columns and subsequent alpha

106 spectrometry measurement. First, two aliquots of uranyl nitrate were prepared containing  
107 0.55 g of pure uranyl (corresponding to 0.260 g of uranium), and labelled as URANYL-1  
108 and URANYL-2. These results were checked against the previous results from the first  
109 group of aliquots.

110 Second, two aliquots were prepared by the hydrothermal reaction of 0.032 g of uranyl  
111 (0.015 g of uranium) with 300 g FEBEX bentonite and 1.1 g of  $\text{ZrO}(\text{NO}_3)_2 \cdot 7\text{H}_2\text{O}$  (as  
112 tetravalent simulator of uranium) (Villa-Alfageme et al., 2014). After the hydrothermal  
113 reaction, the solid and liquid remnant were examined. The solid product aliquot contained  
114 reacted bentonite, zircon silicate and reacted uranium in both phases (labelled as ZrU-  
115 Solid) (Villa-Alfageme et al., 2015). The liquid product aliquot contained dissolved zircon  
116 and uranium (labelled as ZrU-Liquid). Additionally, in order to validate the analysis of the  
117 two aliquots (ZrU-Solid and ZrU-Liquid), a comparison with gamma-ray spectrometry  
118 technique was carried on.

## 119 2.2. *UTEVA chromatographic extraction method*

120 This procedure was adapted from (Mas et al., 2012) for the matrices described and it is  
121 schematized in Fig. 1a.

122

123 1. *Digestion of the solid matrix.* Uranyl samples were digested with concentrated  
124 nitric acid. Whereas bentonites were total digested by a combination of  $\text{HNO}_3$ -  
125  $\text{HCl}$ - $\text{HF}$  (5 mL - 2 mL - 1 mL). Samples were gently heated and stirred until  
126 complete dissolution and taken to dryness. Residue is again dissolved in 15 mL  
127 of 8 mol  $\text{L}^{-1}$  nitric acid.

128 2.  $\text{Fe}^{3+}$  carrier was added and pH raised to 8.5 with ammonium hydroxide to get  
129 the precipitation of iron hydroxides and actinides, the supernatant was removed  
130 by siphoning and discarded after settling for at least 8 h.

- 131 3. UTEVA column was preconditioned loading 3.5 mL of 3 mol L<sup>-1</sup> HNO<sub>3</sub> three  
132 times.
- 133 4. Precipitate was dissolved in 15 mL of 3 mol L<sup>-1</sup> HNO<sub>3</sub>- 1 mol L<sup>-1</sup> Al(NO<sub>3</sub>)<sub>3</sub> and  
134 200 mg ascorbic acid. Dissolved sample was loaded into the resin.
- 135 5. *Elution of Am/Pu/Sr/Po/Ra.* The column was rinsed with 5 mL of 3 mol L<sup>-1</sup>  
136 HNO<sub>3</sub> - 1 mol L<sup>-1</sup> Al(NO<sub>3</sub>)<sub>3</sub>, afterwards with 10 mL of 3 mol L<sup>-1</sup> HNO<sub>3</sub> three  
137 times and finally rinsed with 5 mL of 9 mol L<sup>-1</sup> HCl (Oliveira and Carvalho,  
138 2006).
- 139 6. *Elution of thorium.* Column was rinsed with 4 mL of 5 mol L<sup>-1</sup> HCl - 0.05 mol  
140 L<sup>-1</sup> oxalic acid five times eluting the thorium fraction.
- 141 7. *Elution of uranium.* The column was finally rinsed with 5 mL of 1 mol L<sup>-1</sup> HCl  
142 three times eluting the uranium fraction.

143 2.3. *TBP liquid-liquid solvent extraction method*

144 The procedure followed for the uranium, thorium and polonium separation was adapted  
145 from the TBP procedure described in (Martínez-Aguirre, A., García-León, M., Ivanovich,  
146 1994). It is outlined in Fig. 1b and is in detail below:

147

- 148 1. Pretreatment of the sample was carried out following step 1 described in 2.2.
- 149 2. Uranium was precipitated with iron hydroxide and then taken to dryness on a  
150 hot plate.
- 151 3. The precipitate was dissolved in 10 mL of 8 mol L<sup>-1</sup> HNO<sub>3</sub> and introduced into  
152 a 50 mL funnel for the solvent extraction.
- 153 4. 5 mL TBP were added to the funnel.

- 154 5. *Extraction of polonium.* The funnel was shaken for 15 min and the aqueous  
155 phase removed. Additionally, 10 mL of 8 mol L<sup>-1</sup> HNO<sub>3</sub> were added and the  
156 process repeated. This was repeated three times to get an aqueous final solution  
157 of 30 mL containing the polonium.
- 158 6. 20 mL Xilene were added to the funnel.
- 159 7. *Extraction of thorium.* 15 mL of 1.5 mol L<sup>-1</sup> HCl were added to the funnel and  
160 the solution shaken for 10 minutes. The aqueous phase was removed and the  
161 process was repeated three times to finally obtain 45 mL of HCl solution,  
162 containing thorium (including eventually some traces of uranium).
- 163 8. *Extraction of uranium.* 15 mL of MiliQ water were added and the solution was  
164 shaken for 10 minutes. The aqueous phase was removed and the process was  
165 repeated again three times to get 45 mL of H<sub>2</sub>O solution, containing the uranium  
166 fraction.
- 167 9. *Purification of thorium.* Thorium solution obtained from the solvent extraction  
168 might present traces of uranium, for this reason it was essential to make a final  
169 purification of thorium. This was done by chromatographic separation in a glass  
170 column (height h = 10 cm; diameter 1 cm). 6.5 mL of AG1-X8 resin was added  
171 to the column and preconditioned with 10 mL 9 mol L<sup>-1</sup> of HCl twice. Thorium  
172 solution was taken to dryness, redissolved in 4 x 10 mL of 9 mol L<sup>-1</sup> HCl and  
173 loaded into the column. Resin was rinsed three times with 10 mL of 9 mol L<sup>-1</sup>  
174 HCl. Uranium was retained by resin and a purified Th fraction was recovered  
175 in the eluted solution.

#### 176 2.4. *Alpha-particle spectrometry*

177 Purified uranium and thorium phases were electroplated onto stainless steel discs  
178 (Martínez-Aguirre, A., García-León, M., Ivanovich, 1994) and measured and polonium  
179 was self-deposited onto a silver disk (Le Moigne et al., 2013). Counting of thorium,  
180 uranium (electro-deposited) and polonium (self-deposited) isotopes was done using alpha

181 detector PIPS type (Canberra) in an array comprised of 10 chambers. Measurements were  
182 undertaken at CITIUS (Centro de Investigación, Tecnología e Innovación, Universidad de  
183 Sevilla) laboratory at Universidad de Sevilla. The resolution of the peaks was found to be  
184 between 60 and 40 keV in all cases.

#### 185 2.5. *Gamma-ray spectrometry*

186 The gamma-ray measurements were carried on by a Canberra n-type hyper-pure  
187 germanium gamma-ray detector (HPGe), located at Centro de Investigación, Tecnología e  
188 Innovación Universidad de Sevilla, CITIUS, with a nominal relative photo-peak efficiency  
189 of 60% at 1332 keV. The detector chamber was set up by a lead shield (10 cm thick  
190 standard lead) and an inner copper layer (5 mm) protecting the detector against  
191 environmental background radiation. The electronic chain consisted of a Canberra  
192 preamplifier 2002, and a Canberra Inspector 2000 DSP digital electronic chain. Gamma-  
193 ray spectra were analysed with Genie2K software.

194 Hydrothermal reaction products were collected by filtration using 0.45 µm Milipore filters  
195 and air-dried at 60 °C. In order to measure natural <sup>235</sup>U activity in the sample, the gamma-  
196 ray emission of 143.8 keV (10.9% total yield) was selected.

197 Counting efficiencies were calculated through Monte Carlo simulations using LABSOCS  
198 program (Hurtado and Villa, 2010) for the two counting geometries used: a 0.45 µm  
199 Millipore filter (ZrU-Solid) and a 100 mL cylindrical beaker (ZrU-Liquid). The  
200 composition of the solid sample was essential to compute correctly the simulated efficiency  
201 of this counting geometry.

202 Finally, Monte Carlo efficiencies were successful compared to the experimental ones  
203 obtained through the preparation of solid and aqueous standards spiked with a known  
204 amount of diluted uranyl solution.

#### 205 2.6. *Scanning electron microscopy*

206 The morphology and chemical composition of the hydrothermal products were investigated  
207 using a SEM-FEG HITACHI S-4800 a scanning electron microscope equipped with an



208 Xflash 4010 (BRUKER) for energy dispersive X-ray (EDX) analysis, located at  
209 Microscopy Service in ICMS (CSIC-Universidad de Sevilla).

### 210 **3. Results and discussion**

211 In this section, the obtained activities and isotopic ratios using both radiochemical methods  
212 are shown for each isotope fraction, and a discussion about the chemical recovery, cross-  
213 contamination, and maximum load capacity is carried out.

#### 214 *3.1. Uranium fractions*

215 The results obtained for uranium activity for each aliquot and radiochemical method (TBP  
216 or UTEVA) are presented in Table 1 and Fig. 2. The components contributing to the  
217 combined measurement uncertainty such as count rates of sample and tracer, chemical  
218 recovery, tracer activity and mass of the sample and the tracer are calculated as one  
219 standard deviation.

220 Table 1 shows that both UTEVA column method and TBP method are capable of extracting  
221 the uranium from the analysed aliquot with an acceptable chemical yield. The chemical  
222 yield using the added  $^{232}\text{U}$  internal tracer is around 45% for the solvent extraction method  
223 and 65% for the chromatographic extraction method.

224 With respect to the isotopic ratios, the values obtained for  $^{234}\text{U}$  and  $^{238}\text{U}$  ( $^{234}\text{U}/^{238}\text{U}$ ), and  
225  $^{235}\text{U}$  and  $^{238}\text{U}$  ( $^{235}\text{U}/^{238}\text{U}$ ) are 0.45 and 0.095 respectively. These values do not correspond  
226 to those of natural uranium,  $\sim 1$  and 0.046 respectively (Brennecke et al., 2010). However,  
227 this is in agreement with the values measure in commercial uranium reagents (Iturbe,  
228 1992). Specifically, the  $^{234}\text{U}/^{238}\text{U}$  isotopic ratio for U-UTEVA-2 sample is 20% lower than  
229 the ratios obtained for U-TBP-1, U-TBP-2 and U-UTEVA-1 samples, and it is also 40%  
230 higher for the  $^{235}\text{U}/^{238}\text{U}$  ratio (see Table 1). It can be asserted that this behaviour is not due  
231 to the pre-treatment because this step is common for samples U-TBP-1, U-TBP-2, U-  
232 UTEVA-1 and UTEVA-2. This effect has not been observed in the analysis of  
233 environmental samples following UTEVA method. Further studies should be conducted in  
234 that respect.

235 On the other hand, thorium was not detected in any of the two methods in the  
236 electrodeposited U fraction. Since thorium concentration is very small in uranyl matrices,  
237 thorium contamination in U fraction was evaluated from the analysis of  $^{229}\text{Th}$  tracer.

238 One of the drawbacks of the use of UTEVA resins for uranium analysis is its limitation on  
239 the maximum accepted uranium concentration and its dependence on the type of matrix.  
240 The manufacturer recommends a maximum load capacity of the UTEVA resin  
241 (Triskem Int.) for U is approximately 0.015 g per 2 mL of the pre-packaged UTEVA  
242 columns. In order to check the UTEVA performance several experiments were carried out  
243 using only UTEVA columns for the analysis of two aliquots of pure uranyl (URANYL-1,  
244 URANYL-2). In the experiments with pure uranyl the maximum capacity of the column  
245 for the measurement of U was exceeded, since 0.260 g of uranyl was analysed. The results  
246 in Table 2 show that the chemical yields drop below 1% when exceeding the capacity of  
247 the column. These results indicate that for UTEVA method it is very important not exceed  
248 the load capacity, because the chemical yield decreases drastically, and therefore, an  
249 increase of the resin weight required to analyse samples with high concentration of uranium  
250 is cost-prohibitive.

251 Additionally, as in most analytical situations, the presence of significant concentrations of  
252 matrix elements can affect the proper operation of methods based on UTEVA resin  
253 (Horwitz et al., 1992). Therefore, the performance of these resins was evaluated also in  
254 matrices with high silicate content (high refractory fraction). In order to check the UTEVA  
255 performance several experiments were carried out using only UTEVA columns for the  
256 analysis of two aliquots of zirconium-uranium disilicate, formed after a hydrothermal  
257 treatment with FEBEX and  $\text{ZrO}(\text{NO}_3)_2\text{-UO}_2(\text{NH}_3)_2$  (Villa-Alfageme et al., 2015),  
258 containing the solid fraction (ZrU-Solid) and the liquid one (ZrU-Liquid) (see Section 2.1.  
259 for description).

260 The characterization of the solid fraction was carried out through SEM micrographs of the  
261 reacted FEBEX with  $\text{ZrO}^{2+}$  (Fig. 3). The solid sample shows lamellar particles with a  
262 chemical composition consisting mainly of  $\text{ZrO}^{2+}$  as interlayer cations (Figs. 3a–3d), and  
263 agglomerations of small particles with brilliant appearance (Fig. 3b, point 1) with a

264 chemical composition compatible with phase containing zirconium (Fig. 3e). Moreover,  
265 the SEM/EDX analysis of a different zone (Fig. 3c, point 2) indicated that the treated clay  
266 mineral contain iron, probably released upon degradation of the container (Fig. 3f).

267 Finally, the ZrU-Solid and ZrU-Liquid samples were analysed using both UTEVA  
268 radiochemical method and alpha-particle spectrometry, and gamma-ray spectrometry  
269 technique. This all translates in the results shown in Table 2. The activity of  $^{235}\text{U}$  for ZrU-  
270 Solid and ZrU-Liquid samples through gamma-ray spectrometry was  $7.6\pm 1.5$  Bq and  
271  $3.5\pm 1.4$  Bq respectively. Both methods give results in total agreement validating the use of  
272 UTEVA resin for the analysis of complex matrices.

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### 274 3.2. *Thorium fractions*

275 The results obtained for the concentrations of thorium activity for each aliquot and  
276 radiochemical method are presented in Table 3.

277 Natural thorium is not measured in the Th fraction above the limit of detection through any  
278 of the radiochemical methods. The chemical yields obtained through  $^{229}\text{Th}$  are similar to  
279 those obtained for the U fraction. According to the obtained thorium yields, both methods  
280 are apparently suitable for Th measurements.

281 However, the percentage of U in the Th fraction of the analysed samples has been obtained  
282 and shown in Fig. 4. Note that a significant difference between the two methods (UTEVA  
283 and TBP) is shown in relation to the Th detected. In the samples separated by UTEVA  
284 chromatography columns (U-UTEVA-1 and U-UTEVA-2), U isotopes peaks clearly  
285 appear in the Th fraction contaminating the results. The contamination of U has been  
286 possibly detected because the analysed samples were with higher activities than natural  
287 samples (clay, rock) (about 10 Bq). This contamination of U in the Th fraction is not usually  
288 observed in the analysis of low-level environmental samples by UTEVA method because  
289 the percentage of the initial U activity presented in the spectra of Th was calculated to be  
290 a 1.5% approximately. On the other hand, this contamination does not exist in the samples  
291 separated by the TBP solvent extraction method.

292 Therefore, the U-Th separation procedure using UTEVA columns efficiently separates the  
293 Th fraction from uranium, but about 1.5% of the initial uranium contaminates the Th  
294 fraction (Mas et al., 2012). This is especially relevant in those matrices where the activity  
295 of U is at least one order of magnitude higher than the activity of Th. This contamination  
296 may be drastically reduced using a second chromatographic column in tandem, but this can  
297 mean substantially higher cost. A TEVA column could be attached to the top end of the  
298 UTEVA column, absorbing TEVA resin strongly thorium (IV) from nitric acid solution,  
299 and extracting UTEVA resin all tetravalent actinides, including U, from the same nitric  
300 acid solution.

### 301 3.3. *Polonium fraction*

302 The results obtained for the concentrations of polonium activity for each aliquot and  
303 radiochemical method are presented in Table 4. Radiochemical yields around 55-60% are  
304 obtained for both methods using  $^{209}\text{Po}$  as tracer.

305 It must be highlighted the need to place the silver disk vertically during the autodeposition  
306 process, and finally washing it with acetone and distilled water to avoid the deposition of  
307 U traces on the disk. This is important in this case due to the very high concentration of  
308 uranium in the sample.

309 Finally, traces of natural  $^{210}\text{Po}$  in uranyl samples were detected. The origin is the decay  
310 chain of  $^{238}\text{U}$ . However, high uncertainties for the activities are obtained because these  
311 activities are very close to the minimum detectable activity.

## 312 4. Conclusions

313 The standard TBP method has proven to be an efficient and robust technique to analyse  
314 uranium and thorium concentration for all kinds of samples (either HLRW or low-level  
315 environmental samples). On the other hand, the uranium-thorium separation method using  
316 UTEVA columns works efficiently even applied in complex matrices. However, UTEVA  
317 radiochemical method reaches a total separation of the uranium fraction from thorium  
318 fraction, but a maximum of 1.5% of the initial uranium contaminates the Th fraction. This

319 is especially relevant in those matrices where the concentration of U is orders of magnitude  
320 higher than that of Th. Therefore, further studies should be carried out to elucidate the use  
321 of UTEVA resins in the analysis of HLRW materials.

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338 Tables

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340 **Table 1.** Activity (Bq) and isotopic ratios of the uranium isotopes using the radiochemical  
341 method with TBP (U-TBP-1 and U-TBP-2) and the radiochemical method with UTEVA  
342 (U-UTEVA-1 and U-UTEVA-2). MDA is the Minimum Detectable Activity.

Sample	<sup>234</sup> U (Bq)	± σ	<sup>235</sup> U (Bq)	± σ	<sup>238</sup> U (Bq)	± σ
U-TBP-1	10.8	0.3	2.19	0.07	23.6	0.7
U-TBP-2	10.7	0.3	2.18	0.07	23.4	0.7
U-UTEVA-1	9.9	0.3	2.18	0.07	22.1	0.7
U-UTEVA-2	9.0	0.3	3.25	0.10	23.9	0.7

Sample	<sup>234</sup> U/ <sup>238</sup> U	<sup>235</sup> U/ <sup>238</sup> U	<sup>232</sup> U recovery	MDA <sup>234</sup> U (Bq)	MDA <sup>235</sup> U (Bq)	MDA <sup>238</sup> U/ (Bq)
U-TBP-1	0.46	0.093	44%	0.05	0.08	0.06
U-TBP-2	0.46	0.093	47%	0.05	0.07	0.06
U-UTEVA-1	0.45	0.099	63%	0.04	0.08	0.05
U-UTEVA-2	0.38	0.136	65%	0.05	0.09	0.05

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355 **Table 2.** Activity (Bq) and isotopic ratios (in activity) of the uranium isotopes using the  
 356 UTEVA radiochemical method for pure uranyl matrices (URANYL-1 and URANYL-2)  
 357 and the product of a hydrothermal treatment with FEBEX and  $\text{ZrO}(\text{NO}_3)_2\text{-UO}_2(\text{NH}_3)_2$  in  
 358 the solid fraction (ZrU-Solid) and liquid (ZrU-Liquid). Chemical yields are not included  
 359 for samples under hydrothermal treatment, since most of the uranium is lost in that process,  
 360 not during the radiochemical procedure. MDA is the Minimum Detectable Activity.

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Sample	$^{234}\text{U}$ (Bq)	$\pm \sigma$	$^{235}\text{U}$ (Bq)	$\pm \sigma$	$^{238}\text{U}$ (Bq)	$\pm \sigma$
URANYL-1	666	79	144	17	1541	183
URANYL-2	548	92	78	13	1120	189
ZrU-Solid	52.9	2.4	7.9	0.4	109.3	5.0
ZrU-Liquid	16.1	4.6	3.0	0.7	36.2	7.1
Sample	$^{234}\text{U}/^{238}\text{U}$	$^{235}\text{U}/^{238}\text{U}$	$^{232}\text{U}$ recovery	MDA $^{234}\text{U}$ (Bq)	MDA $^{235}\text{U}$ (Bq)	MDA $^{238}\text{U}/$ (Bq)
URANYL-1	0.432	0.0938	0.54%	0.05	0.08	0.06
URANYL-2	0.489	0.0695	0.30%	0.05	0.07	0.06
ZrU-Solid	0.485	0.0723	--	0.04	0.08	0.05
ZrU-Liquid	0.446	0.0830	--	0.05	0.09	0.05

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369 **Table 3.** Activity (Bq) of thorium isotopes using the radiochemical procedure with TBP  
 370 (U-TBP-1 and U-TBP-2) and the radiochemical process with UTEVA (U-UTEVA-1 and  
 371 U-UTEVA-2). The chemical recovery is shown through  $^{229}\text{Th}$ . MDA is the Minimum  
 372 Detectable Activity.

Sample	$^{230}\text{Th}$ (Bq)	$\pm \sigma$	$^{232}\text{Th}$ (Bq)	$\pm \sigma$	$^{229}\text{Th}$ recovery	MDA $^{230}\text{Th}$ (Bq)	MDA $^{232}\text{Th}$ (Bq)
U-TBP-1	< MDA		< MDA		60	0.12	0.06
U-TBP-2	< MDA		< MDA		52	0.04	0.05
U-UTEVA-1	< MDA		< MDA		71	0.07	0.03
U-UTEVA-2	< MDA		< MDA		51	0.05	0.05

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387 **Table 4.** Activity (Bq) of  $^{210}\text{Po}$  using the radiochemical procedure with TBP (U-TBP-1  
388 and U-TBP-2) and the chemical procedure with UTEVA (U-UTEVA-1 and U-UTEVA-2).  
389 MDA is the Minimum Detectable Activity.

Sample	$^{210}\text{Po}$ (Bq)	$\pm \sigma$	MDA (Bq)
<b>U-TBP-1</b>	0.00025	0.00013	0.00024
<b>U-TBP-2</b>	0.00064	0.00017	0.00021
<b>U-UTEVA-1</b>	0.00069	0.00017	0.00016
<b>U-UTEVA-2</b>	0.00045	0.00011	0.00016

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397 Table captions

398 **Table 1.** Activity (Bq) and isotopic ratios of the uranium isotopes using the  
399 radiochemical method with TBP (U-TBP-1 and U-TBP-2) and the radiochemical method  
400 with UTEVA (U-UTEVA-1 and U-UTEVA-2). MDA is the Minimum Detectable  
401 Activity.

402 **Table 2.** Activity (Bq) and isotopic ratios (in activity) of the uranium isotopes using the  
403 UTEVA radiochemical method for pure uranyl matrices (URANYL-1 and URANYL-2)  
404 and the product of a hydrothermal treatment with FEBEX and  $\text{ZrO}(\text{NO}_3)_2\text{-UO}_2(\text{NH}_3)_2$  in  
405 the solid fraction (ZrU-Solid) and liquid (ZrU-Liquid). Chemical yields are not included  
406 for samples under hydrothermal treatment, since most of the uranium is lost in that  
407 process, not during the radiochemical procedure. MDA is the Minimum Detectable  
408 Activity.

409 **Table 3.** Activity (Bq) of thorium isotopes using the radiochemical procedure with TBP  
410 (U-TBP-1 and U-TBP-2) and the radiochemical process with UTEVA (U-UTEVA-1 and  
411 U-UTEVA-2). The chemical recovery is shown through  $^{229}\text{Th}$ . MDA is the Minimum  
412 Detectable Activity.

413 **Table 4.** Activity (Bq) of  $^{210}\text{Po}$  using the radiochemical procedure with TBP (U-TBP-1  
414 and U-TBP-2) and the chemical procedure with UTEVA (U-UTEVA-1 and U-UTEVA-  
415 2). MDA is the Minimum Detectable Activity.

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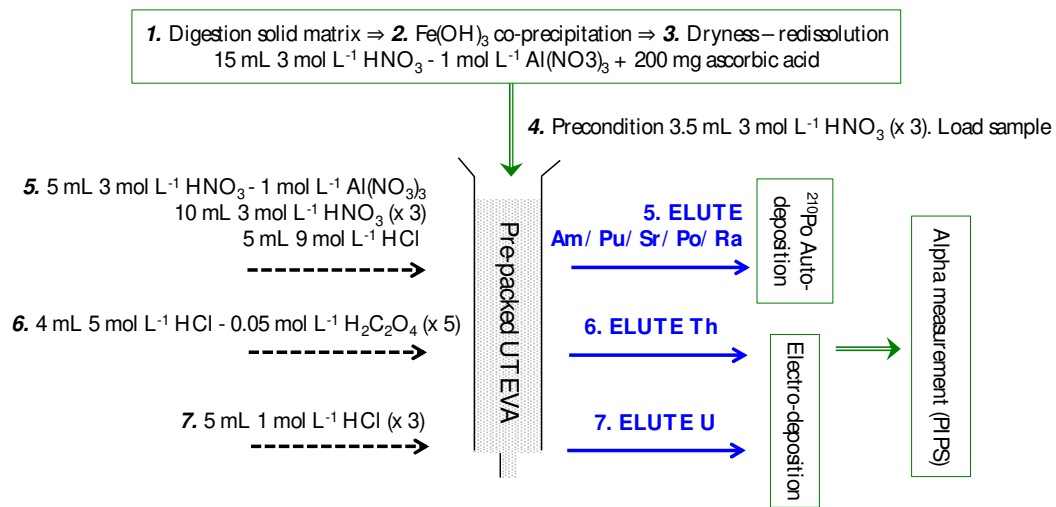
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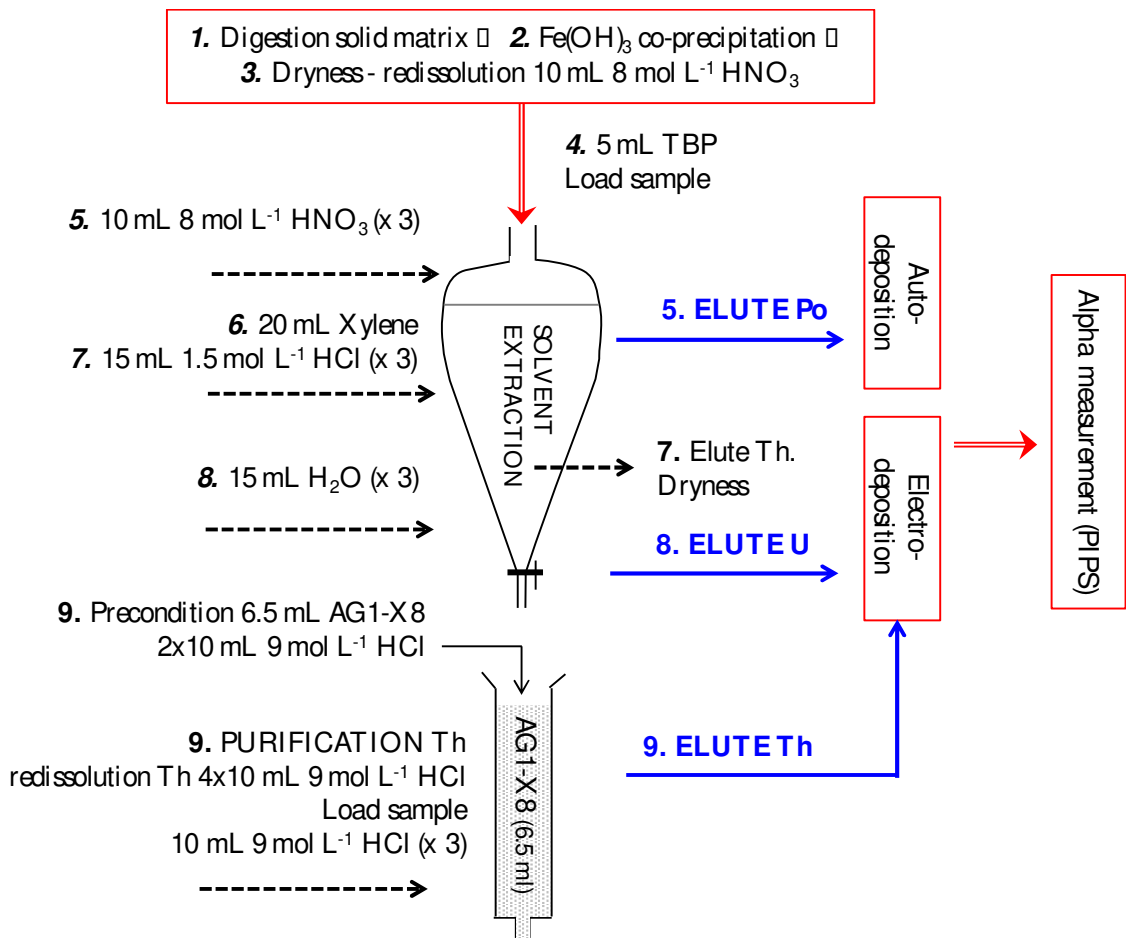


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426 **Fig. 1a.** UTEVA chromatographic extraction method.

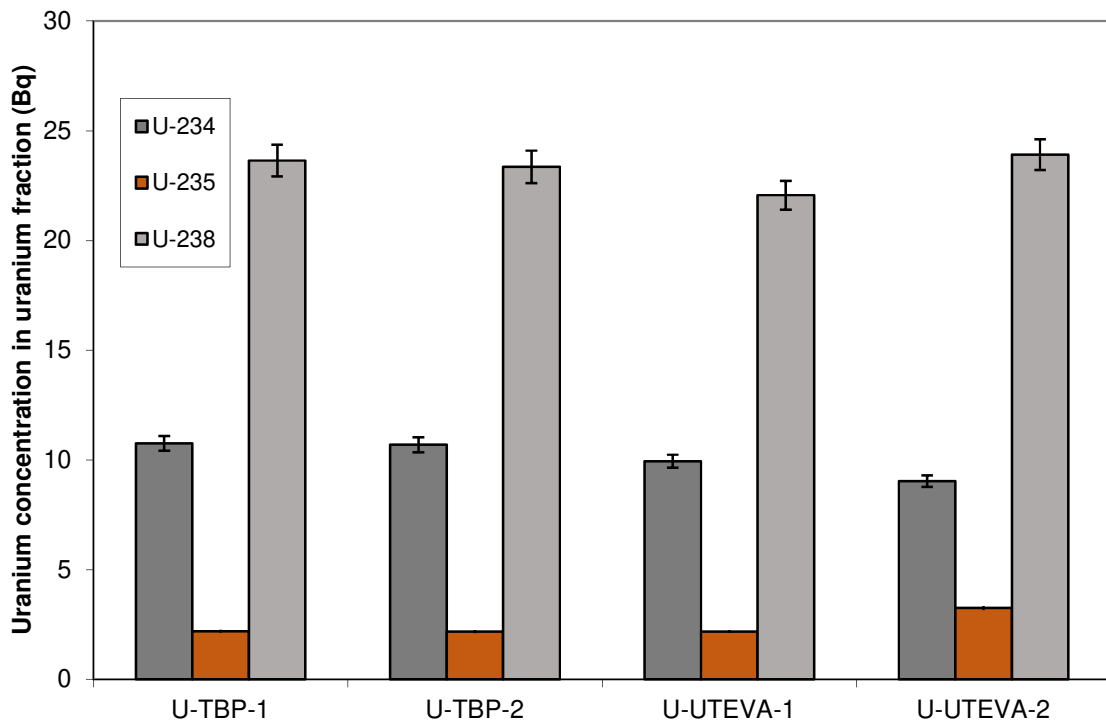
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430 **Fig. 1b.** TBP liquid-liquid solvent extraction method.



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432 **Fig. 2.** Activity concentration (Bq) and isotopic ratios of the uranium isotopes using the  
 433 radiochemical method with TBP (U-TBP-1 and U-TBP-2) and the radiochemical method  
 434 with UTEVA (U-UTEVA-1 and U-UTEVA-2).

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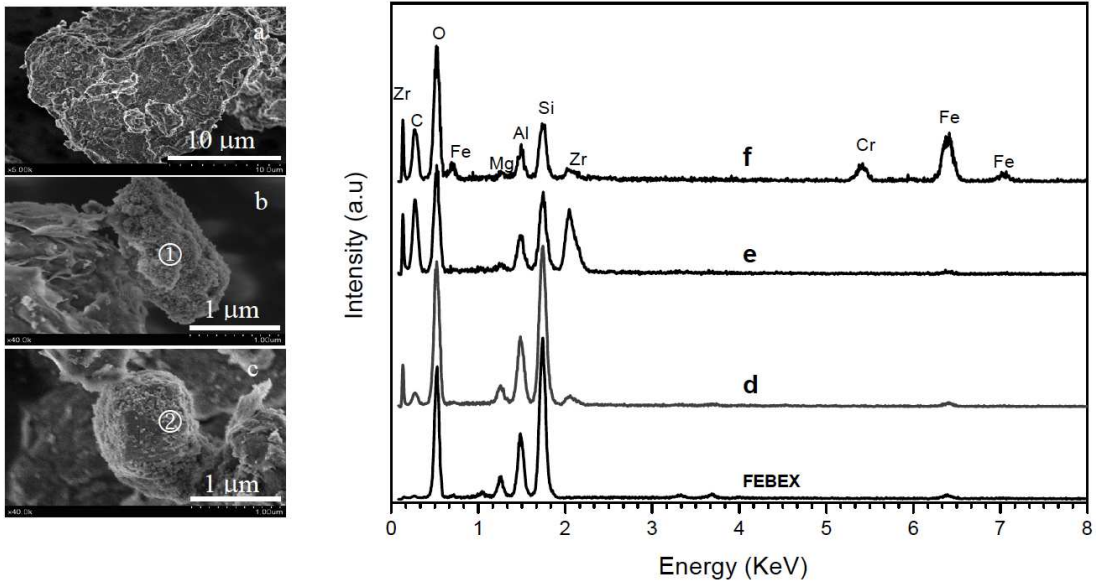
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443 **Fig. 3.** SEM micrographs of the reacted FEBEX with a solution of  $ZrO^{2+}$ : (a) a general  
 444 view; (b) bright particles agglomerates mainly made up of zirconium oxide ion; and (c)  
 445 iron particles coming from container degradation. EDX spectra of: (d) lamellar particles;  
 446 (e) zirconium agglomerates; (f) iron particles; and a FEBEX spectrum as reference.

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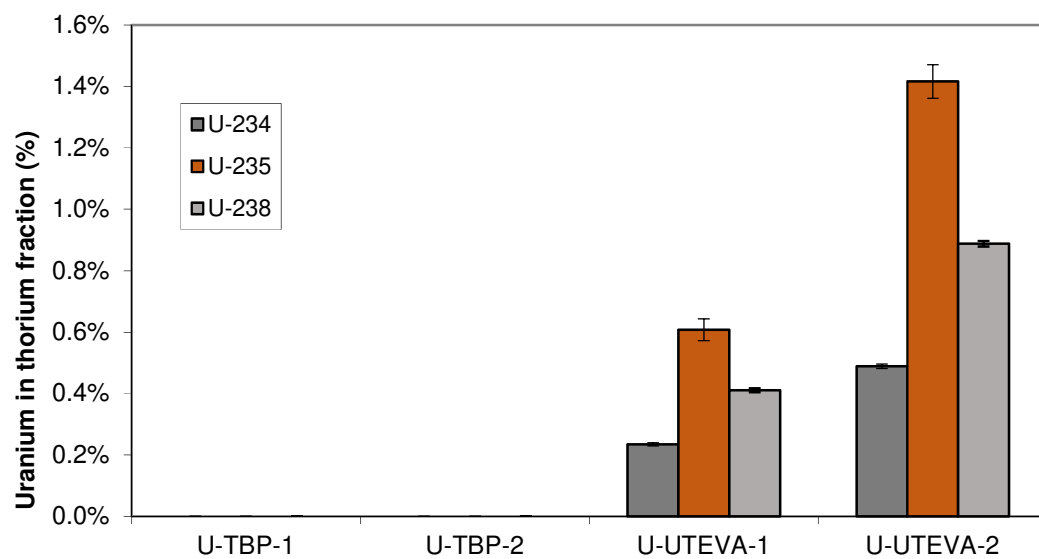
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458 **Fig. 4.** Percentage of uranium measured in thorium fraction in uranyl aliquots measured by  
459 TBP (U-TBP-1 and U-TBP-2) and UTEVA (U-UTEVA-1 and U-UTEVA-2).

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469 Figure captions

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471 **Fig. 1a.** UTEVA chromatographic extraction method.

472

473 **Fig. 1b.** TBP liquid-liquid solvent extraction method.

474

475 **Fig. 2.** Activity concentration (Bq) and isotopic ratios of the uranium isotopes using the  
476 radiochemical method with TBP (U-TBP-1 and U-TBP-2) and the radiochemical method  
477 with UTEVA (U-UTEVA-1 and U-UTEVA-2).

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480 view; (b) bright particles agglomerates mainly made up of zirconium oxide ion; and (c)  
481 iron particles coming from container degradation. EDX spectra of: (d) lamellar particles;  
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485 TBP (U-TBP-1 and U-TBP-2) and UTEVA (U-UTEVA-1 and U-UTEVA-2).

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